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주최 한국통신학회 마이크로파 및 전파 연구회
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후원 (주) 창성, 애드모텍, 에이스테크놀로지,
담스테크, HCT, 맨앤티

협찬 알트소프트, 이너트론, 에이스웨이브텍



Session E

전자장, 해석 1

좌장 : 이왕상 박사 (한국철도기술연구원)

해석1-1 13:15-13:30	Analysis of WPT System using Transient Circuit Theory 97 Hyunjin Shimo, Jongmin Park, Sangwook Nam 서울대학교
해석1-2 13:30-13:45	열차 위치검지용 근거리 무선전력시 오정렬에 따른 전송효율 분석 98 이왕상, 박성수, 이재호 한국철도기술연구원(Korea Railroad Research Institute)
해석1-3 13:45-14:00	A Study of the Effect of Phase Difference between Multiple Transmitters in Wireless Power Transfer System 99 Pengfei Kong, Wonshil Kang, Jae Yong Seong, and Hyunchul Ku Dept. of Electrical Engineering, Konkuk University
해석1-4 14:00-14:15	시간-주파수 해석법을 활용한 근접장 무침 태그 인식 기법 100 이원석, 박지훈, 오경섭*, 유종원 한국과학기술원, *(주)감마누
해석1-5 14:15-14:30	EMC Technologies on EM Wave Absorbers in Korea 101 김동일, 김정창, 길경석, 양규식 한국해양대학교
해석1-6 14:30-14:45	Biconical 구조를 이용한 광대역 흡수체 102 이준호, 이범선 경희대학교

전자장, 해석 2

좌장 : 강진섭 박사 (KRISS)

해석2-1 14:55-15:10	기하 광학 및 확률을 이용한 경로 손실 모델이 적용된 WINNER 채널 모델 103 박찬주, 김우중, 윤영중 연세대학교
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해석2-4 15:40-15:55	ILDC와 저주파 해석방법을 이용한 아주 가는 gap, crack 산란 해석 정확도 검증 106 이현수, 고일석 인하대학교
해석2-5 15:55-16:10	인체신호 검출을 위한 전파 특성 연구 107 장동원, 최재익 한국전자통신연구원

Analysis of WPT System using Transient Circuit Theory

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I. Introduction

The coupled-mode theory (CMT) is one of the models used to characterize a WPT system in steady-state by physicists at MIT [1]. However, it was shown that CMT does not give an accurate transient solution to the WPT system in low Q cases [2]. In this paper, we show transient circuit analysis can be used to define an analytic criterion of magnetic resonance coupling and inductive coupling.

II. Transient circuit analysis

Consider KVL in the equivalent short-circuit of the two identical coupled resonators [2].

$$\begin{aligned} \frac{1}{C} \int I_1(t) dt + (R_1 + R_2) I_1(t) + L_1 \frac{dI_1(t)}{dt} + M \frac{dI_2(t)}{dt} &= 0 \\ \frac{1}{C} \int I_2(t) dt + (R_2 + R_1) I_2(t) + L_2 \frac{dI_2(t)}{dt} + M \frac{dI_1(t)}{dt} &= 0 \end{aligned} \quad (1)$$

characteristic equation in s-domain can be obtained using Laplace transform.

$$\left(s^2 + \left(\frac{\omega}{Q} + \frac{\omega}{Q_{ext}} \right) s + \omega^2 \right) = k_{12}^2 s^4 \quad (2)$$

the current of each resonator can be obtained using basis of Eq. (2) where Q_{ext} is the external Q of the resonator.

$$\begin{aligned} I_1(t) = e^{-\frac{1}{2} \left(\frac{\omega}{Q} + \frac{\omega}{Q_{ext}} \right) t} & \left[\frac{I_0}{2} \cos \left(\frac{\omega \sqrt{4(1-k_{12}) - \left(\frac{\omega}{Q} + \frac{\omega}{Q_{ext}} \right)^2}}{2(1+k_{12})} t \right) + \frac{I_0}{4Q} \sin \left(\frac{\omega \sqrt{4(1-k_{12}) - \left(\frac{\omega}{Q} + \frac{\omega}{Q_{ext}} \right)^2}}{2(1+k_{12})} t \right) \right] \\ + e^{-\frac{1}{2} \left(\frac{\omega}{Q} + \frac{\omega}{Q_{ext}} \right) t} & \left[\frac{I_0}{2} \cos \left(\frac{\omega \sqrt{4(1+k_{12}) - \left(\frac{\omega}{Q} + \frac{\omega}{Q_{ext}} \right)^2}}{2(1+k_{12})} t \right) - \frac{I_0}{4Q} \sin \left(\frac{\omega \sqrt{4(1+k_{12}) - \left(\frac{\omega}{Q} + \frac{\omega}{Q_{ext}} \right)^2}}{2(1+k_{12})} t \right) \right] \end{aligned} \quad (3)$$

the total energy in the resonator is the sum of electric in inductor and magnetic energy in capacitor.

$$E_i(t) = \frac{1}{2} L |i_i(t)|^2 + \frac{1}{2C} \left| \int I_i(t) dt \right|^2 \quad (4)$$

In this paper, a criterion is introduced by how much of the energy is received back after the first resonator once transmits energy. If the received energy of the first resonator after one period (1T) is greater than e^{-3} times of the initially transmitted energy (i.e., $|k_{12}(1T)| > |k_{12}(0)|^2 \cdot e^{-3}$), the WPTS system is considered to be magnetic resonance coupling. The reason of e^{-3}

factor is based on 5% energy rate between two resonators. However, If the received energy after one period is less than e^{-3} times of the first value, which means that the first resonator does not receive back any energy after one period has passed, the WPTS system is under the condition of inductive coupling. The energy in the first and second resonator as a function of time at each sources are shown in Fig. 1,2.

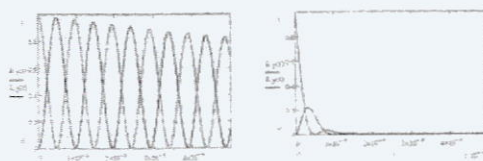


Figure 1,2. Normalized energy in each resonator as function of time when $R_{ext}=0, 50 \text{ ohm}$.

As Fig. 1(a), (b), the results of the energy relation satisfy the condition proposed in previous section.

III. Conclusion

An analytic criterion of magnetic resonance coupling and inductive coupling in WPTS under transient circuit analysis using power sources is proposed. Using the proposed definition, these two terms can be clarified analytically.

Acknowledgement

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References

- [1] A. Karalis, J. D. Joannopoulos, and M. Soljacic, "Efficient wireless non-radiative mid-range energy transfer," *Ann. Phys.*, vol. 323, no. 1, pp. 34-48, Jan. 2008.
- [2] M. Kiani, M. Ghovanloo, "The circuit theory behind coupled-mode magnetic resonance-based wireless power transmission", *IEEE Trans. on Circuits and Systems I: Regular Papers*, vol. 59, pp. 2065-2074, 2012.